

A GEOMETRIC APPROACH TO ROBOTIC MANIPULATION IN PHYSICAL HUMAN-ROBOT INTERACTION

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KUKA

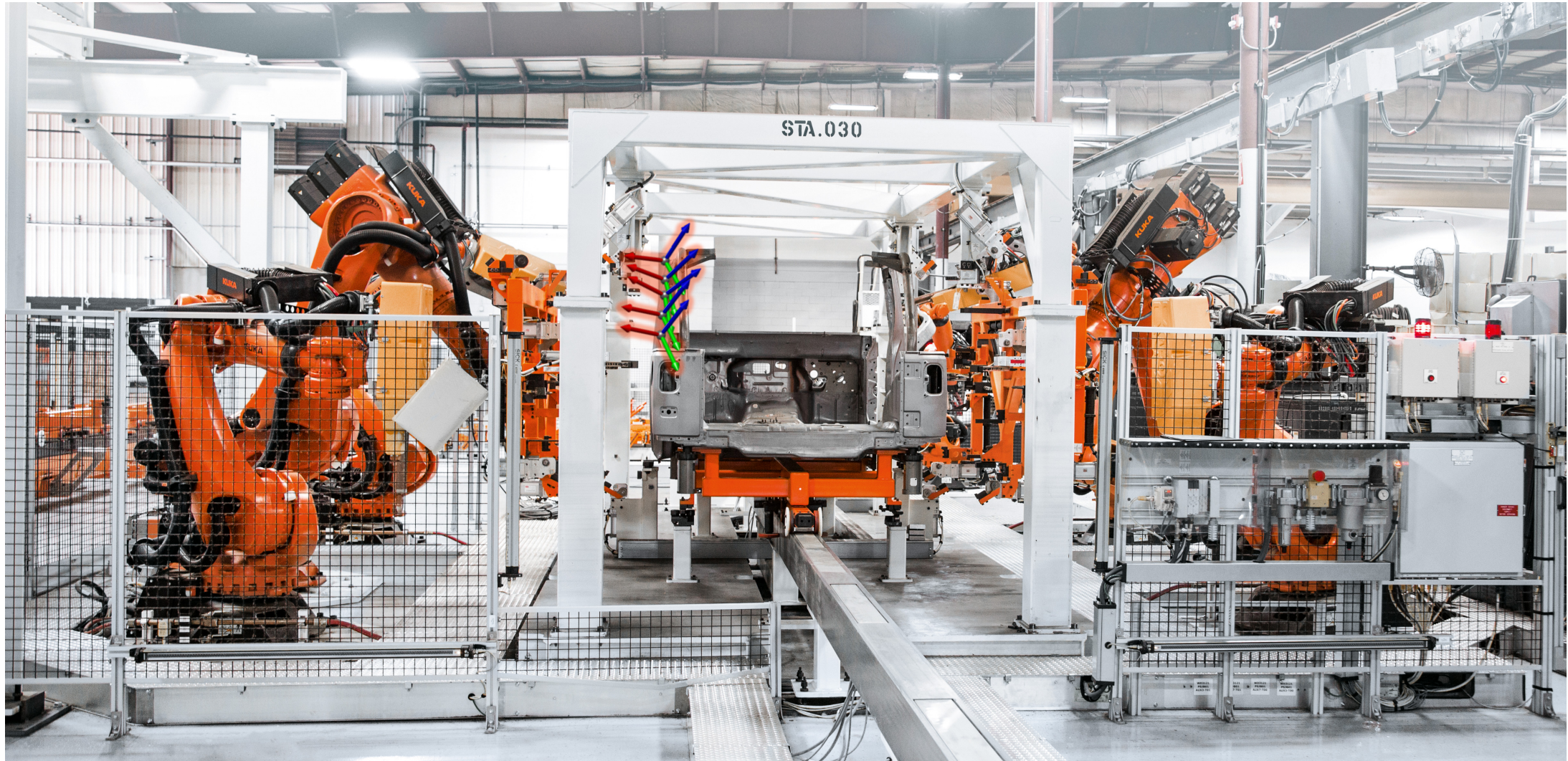


Massachusetts
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Technology

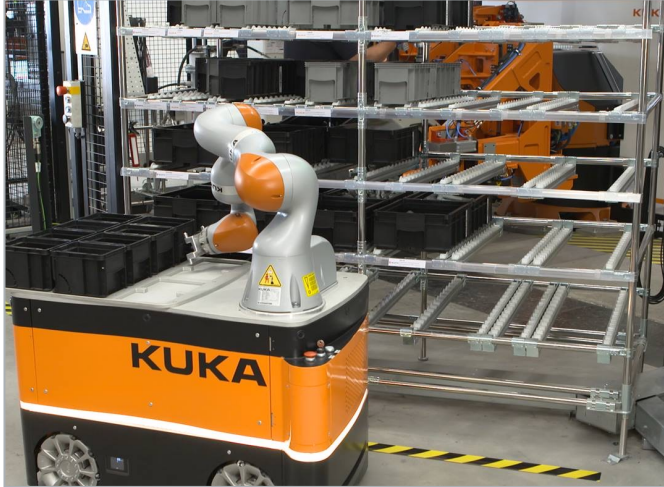


My world of robotics 2013

Source: <https://www.kuka.com/>



My world of robotics 2014 - 2017



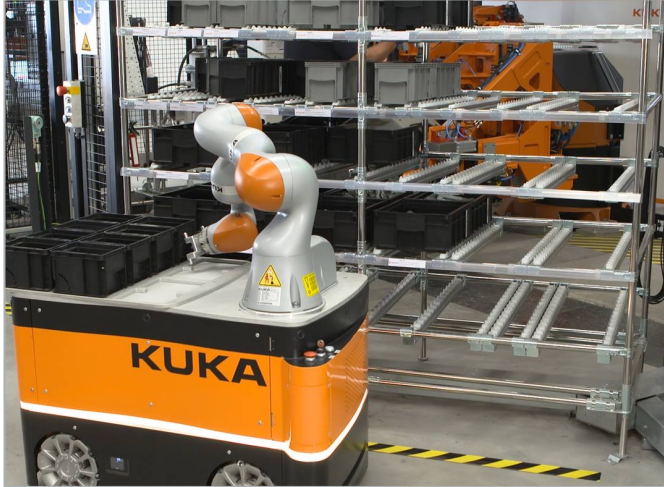
Source: KUKA



Three main challenges:

- 6D-frames impede programming
- Kinematic redundancy not easy to use
- Coordinate choices for safety implementation are crucial

My world of robotics 2018 - now

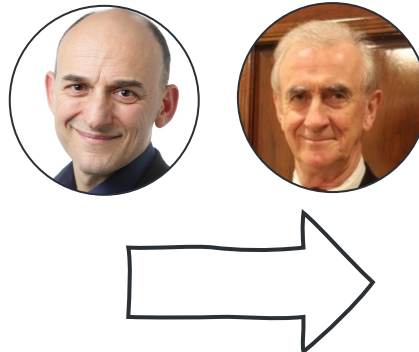


Source: KUKA



Three main challenges:

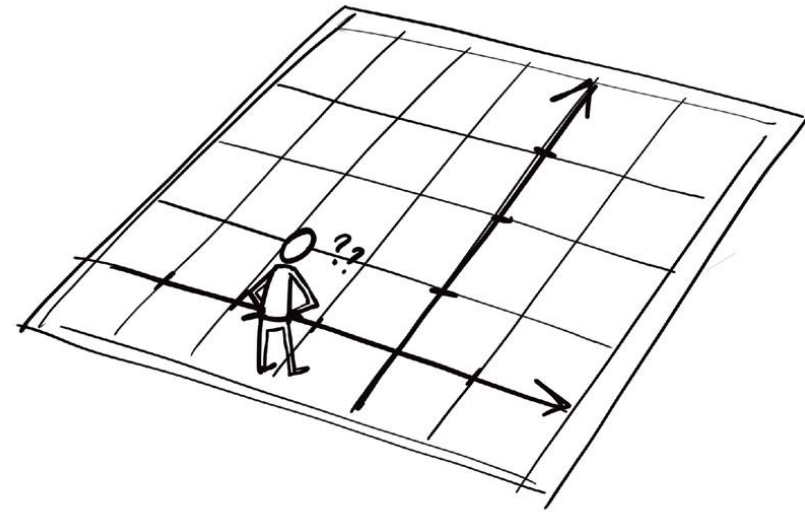
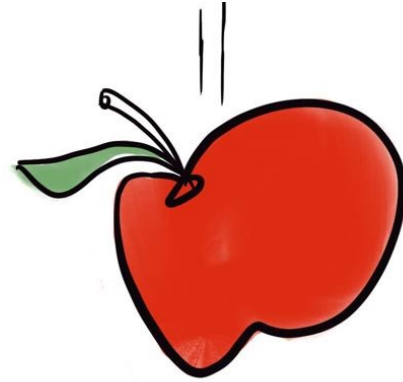
- 6D-frames impede programming
- Kinematic redundancy not easy to use
- Coordinate choices for safety implementation are crucial



Research questions of my thesis:

- Can a robot fulfil one or even multiple tasks?
- How can we realize an efficient and stable robot (multi-task) control?
- How can we facilitate the safety programming for physical Human-Robot Interaction?

I. Dexterity: single task

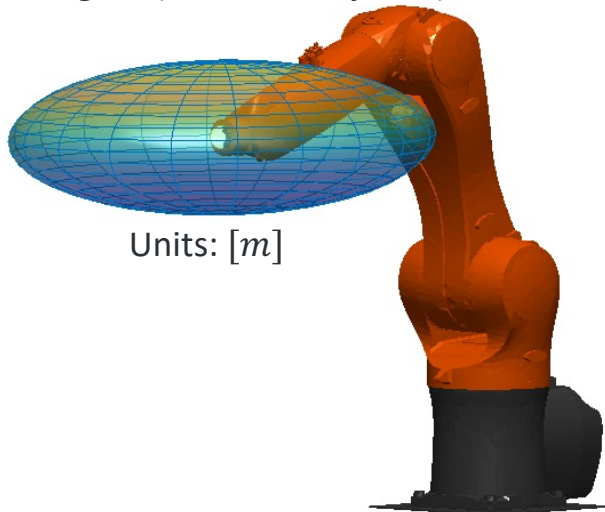


Problem statement: Coordinate dependency of dexterity measures

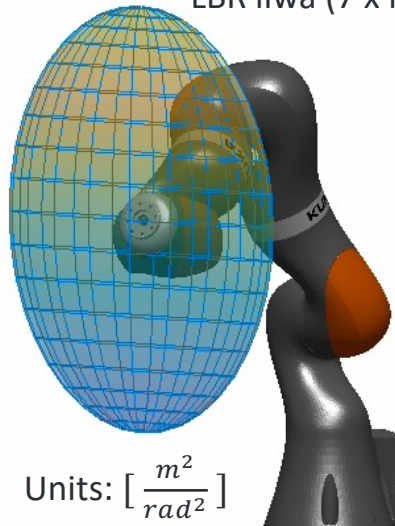
- Dexterity is strongly related to the Jacobian matrix $J(\mathbf{q}) = \begin{pmatrix} J(\mathbf{q})_p \\ J(\mathbf{q})_w \end{pmatrix}$
- Workspace ellipsoid: $\dot{\mathbf{p}}^T (J(\mathbf{q})J(\mathbf{q})^T)^{-1} \dot{\mathbf{p}} = 1$ (Yoshikawa, 1985)
- Shape and orientation of ellipsoid: Eigenvectors and Eigenvalues of $J(\mathbf{q})J(\mathbf{q})^T$

-
- Involves choice for a Generalized Inverse of $J(\mathbf{q})$: $J(\mathbf{q})^\# = W^{-1}J(\mathbf{q})^T(J(\mathbf{q})W^{-1}J(\mathbf{q})^T)^{-1}$
 - A common choice is: $W^{-1} = I$ (Identity) \rightarrow Moore-Penrose Inverse
 - Problem 1: different choices for W^{-1} lead to different manipulability results (Lachner et al., 2020)

Agilus (6 x revolute joints)



LBR iiwa (7 x revolute joints)

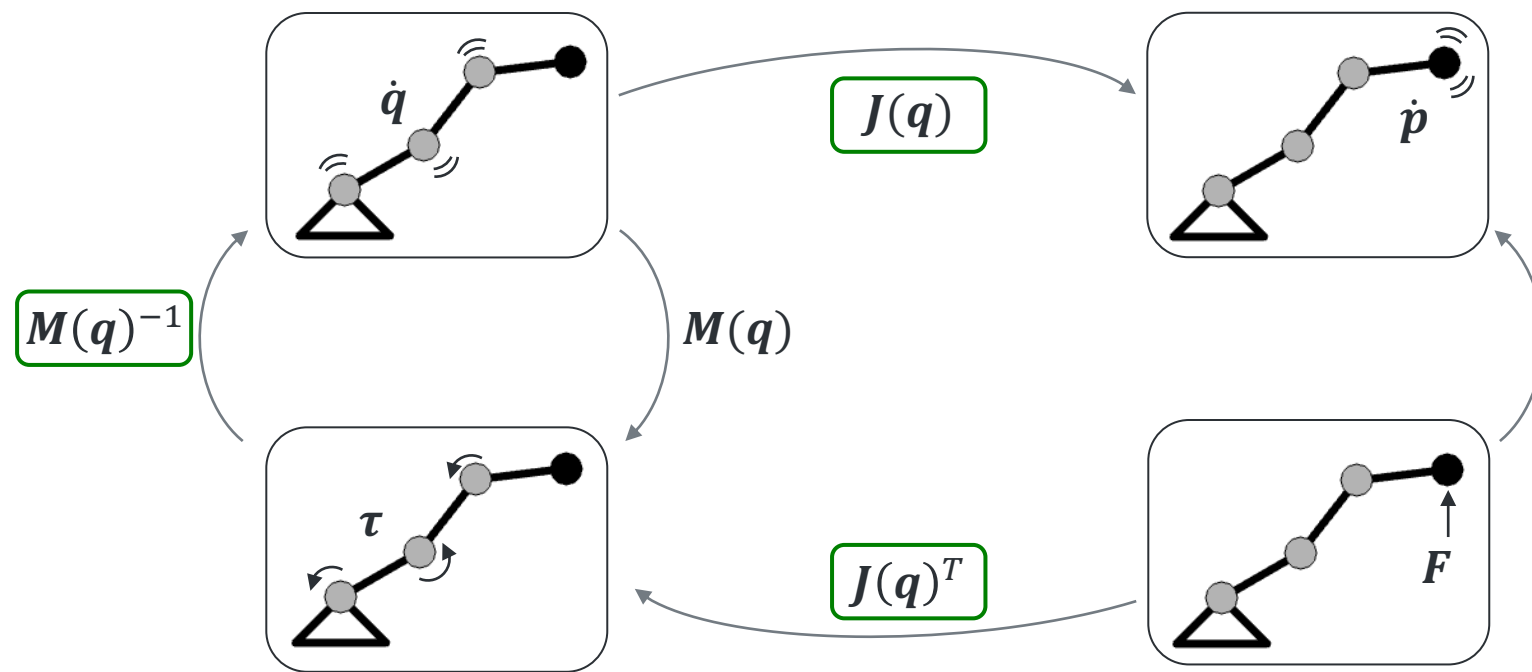


YouBot (3 x prismatic joints, 5 x revolute joints)

Problem 2: Mismatch of units arises!
(Lachner et al., 2020)



Finding: Consistent mapping between robotic spaces

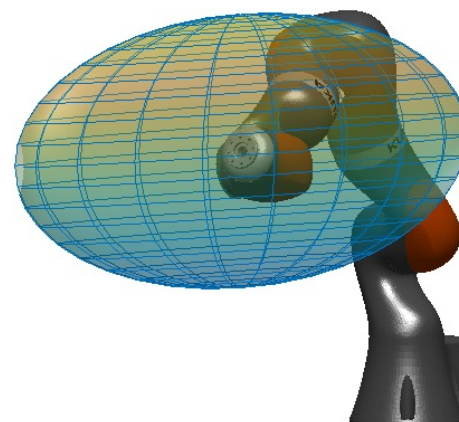
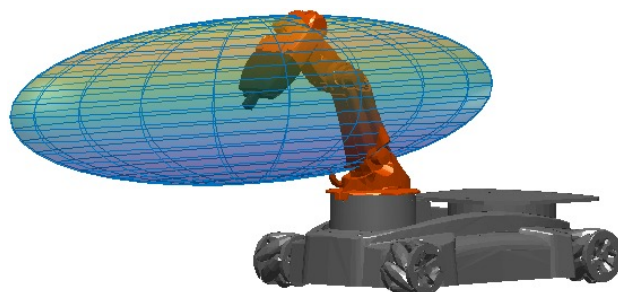
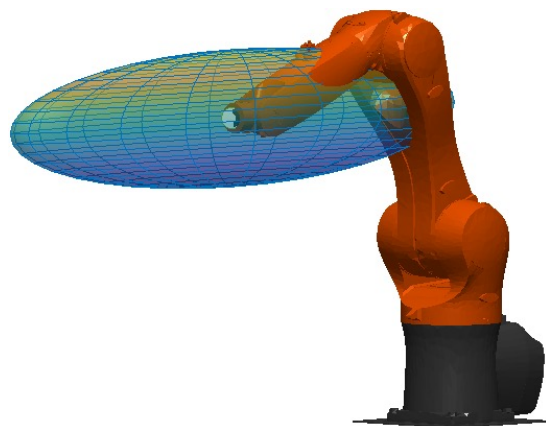


Additional contributions:

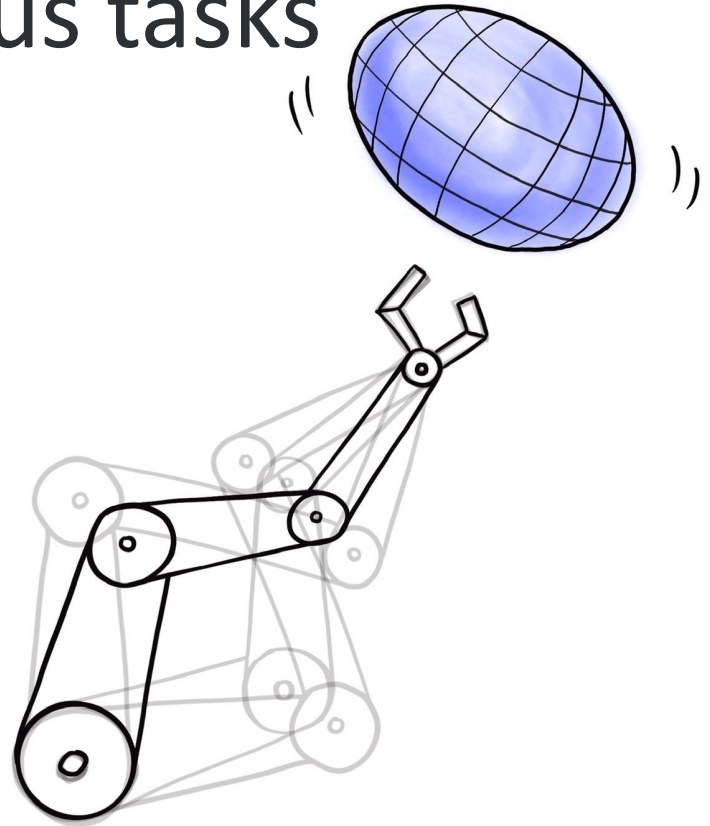
- Generalization for $se(3)$ (twists and wrenches)

$$\Lambda(q)^{-1} = J(q) \overbrace{M(q)^{-1}}^{W^{-1}} J(q)^T$$

- Induced metric $\Lambda(q)^{-1}$ (Lachner et al., 2020)
- Meaningful choice for W^{-1}
- Equal units: $1/[kg]$
- Works for all robots!



II. Dexterity: multiple simultaneous tasks



Problem statement: Task conflicts and their detection

- Impedance Control: Multiple impedances can be superimposed (Hogan, 1985)
- Impedance superposition might yield task conflicts (Hermus, Lachner et al., 2022)
- Nullspace projection can resolve the task conflict (Khatib, 1987)
- Important for industry: know that a task will be sacrificed before it happens

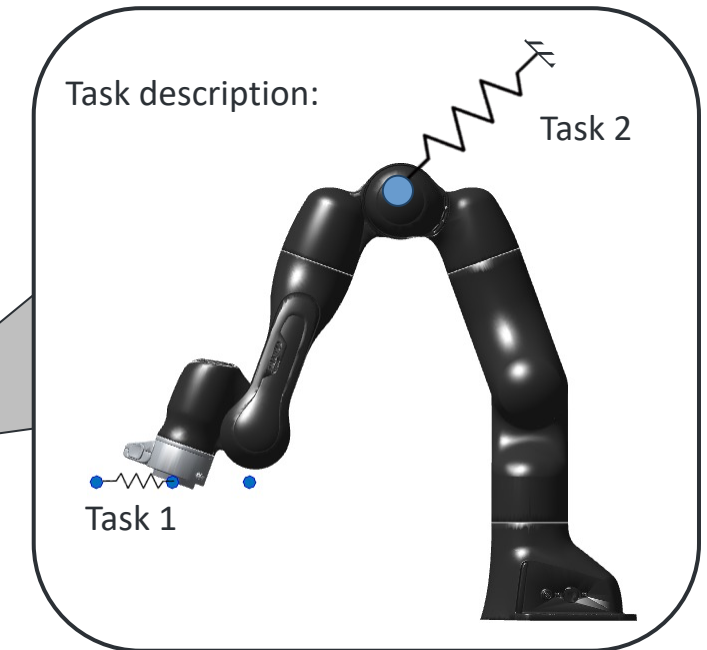
$$\begin{array}{cc} \text{Task 1} & \text{Task 2} \\ \downarrow & \downarrow \\ \tau_{net} = \tau_1 + \tau_2 \end{array}$$

$$\tau_{net} = \tau_1 + \mathbf{N}_1 \tau_2$$

Nullspace Projection:



Impedance Superposition:



Finding: Prediction of conflicts between simultaneous tasks

- Nullspace projection: $\tau_{net} = \tau_1 + \mathbf{N}_1 \tau_2$
 $= \tau_1 + \underbrace{\mathbf{N}_1 \mathbf{J}_2(\mathbf{q})^T}_{\text{Task-consistent Jacobian}} \mathbf{F}_2$

Task-consistent Jacobian: $\mathbf{J}_2^{TC}(\mathbf{q}) = \mathbf{J}_2(\mathbf{q}) \mathbf{N}_1^T$ (Khatib and Sentis, 2004)

- Task-consistent Jacobian drops rank during task conflict with task 1

-
- But: Dependent on joint types (units)

- From first result: $\Lambda_2(\mathbf{q})^{-1} = \mathbf{J}_2(\mathbf{q}) \mathbf{M}(\mathbf{q})^{-1} \mathbf{J}_2(\mathbf{q})^T$
 $\Lambda_2^{TC}(\mathbf{q})^{-1} = \mathbf{J}_2^{TC}(\mathbf{q}) \mathbf{M}(\mathbf{q})^{-1} \mathbf{J}_2^{TC}(\mathbf{q})^T$
 \rightarrow Independent on joint types (Schettino, Lachner et al., 2020)
 \rightarrow Physical quantity: $\left[\frac{1}{kg} \right]$

- For a given direction \mathbf{u} :

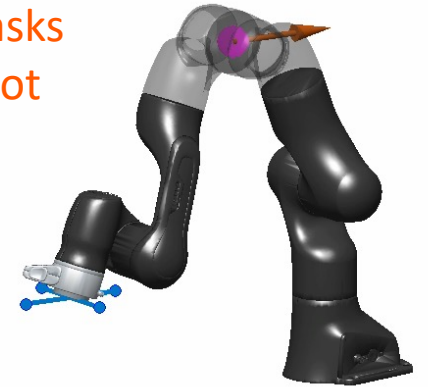
$$m_{TC} = (\mathbf{u}^T \Lambda_2^{TC}(\mathbf{q})^{-1} \mathbf{u})^{-1}$$

- Intuition: virtual mass counteracting task 1** (Lachner et al., 2022)
- Task conflict can be related to the robot weight (or payload)
- In this example, conflict if: $m_{TC} > \frac{1}{2} m_{payload}$

Additional contributions :

- Extension for rotational tasks
- Experiments on a real robot

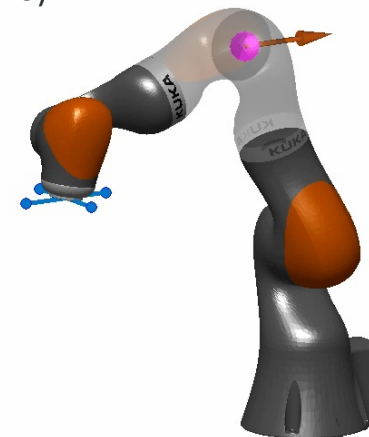
$m_{tc} = 1.0998 \text{ (kg)}$



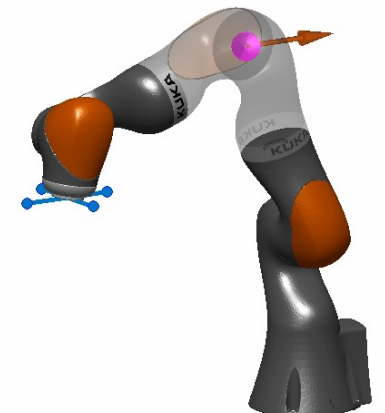
Franka, 3 kg payload

$m_{tc} = 5.3148 \text{ (kg)}$

$m_{tc} = 3.4755 \text{ (kg)}$

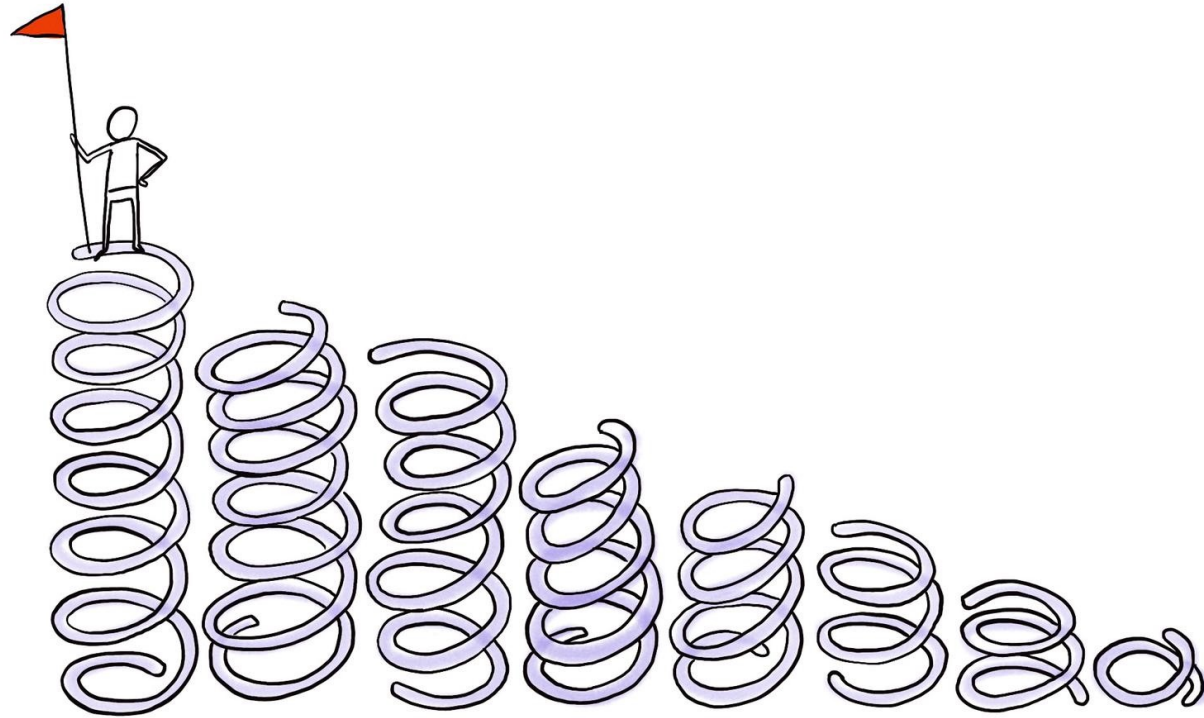


LBR iiwa, 14 kg payload



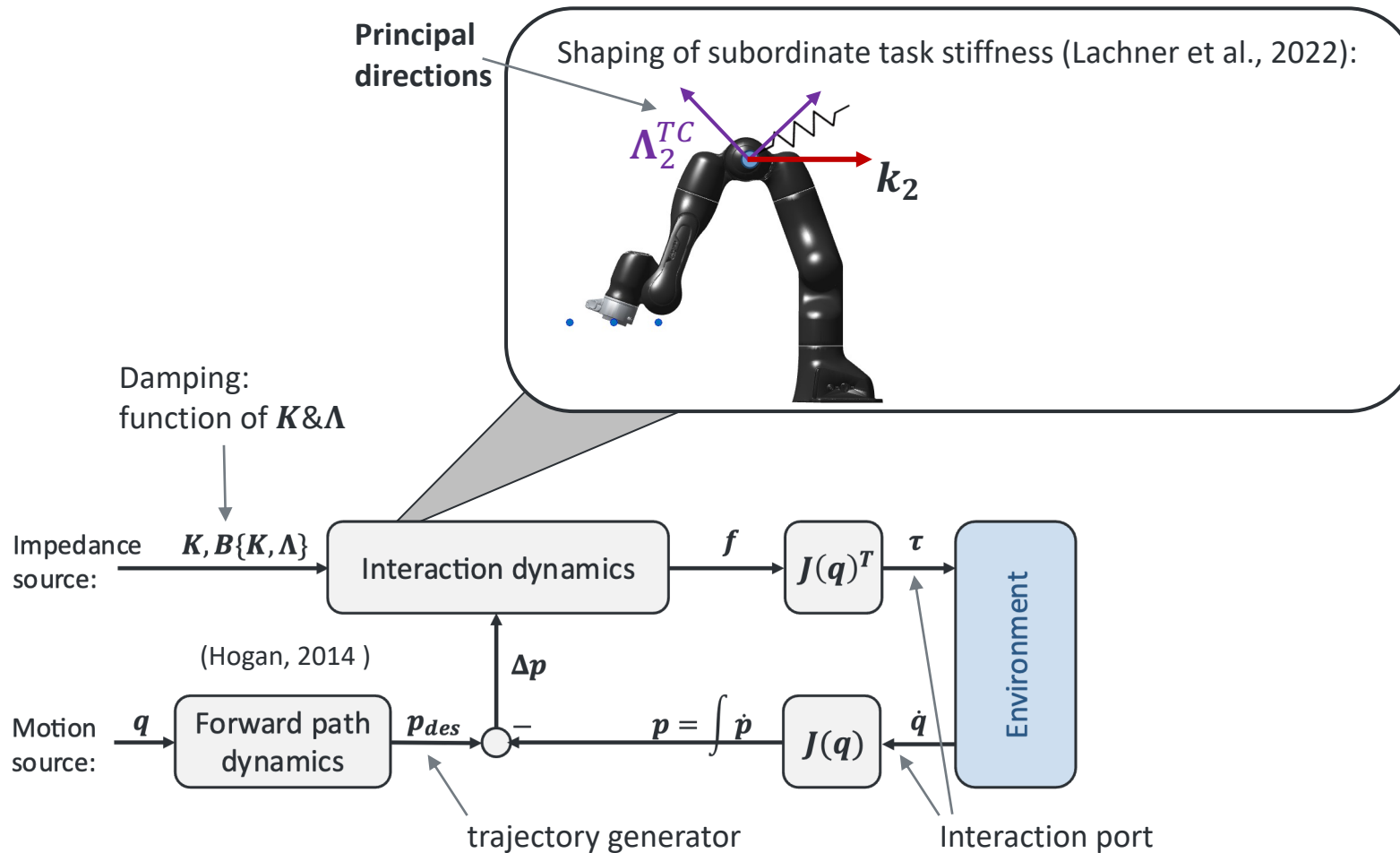
LBR iiwa, 7 kg payload

III. Multi-task impedance control



Finding: Impedance shaping for multi-task control

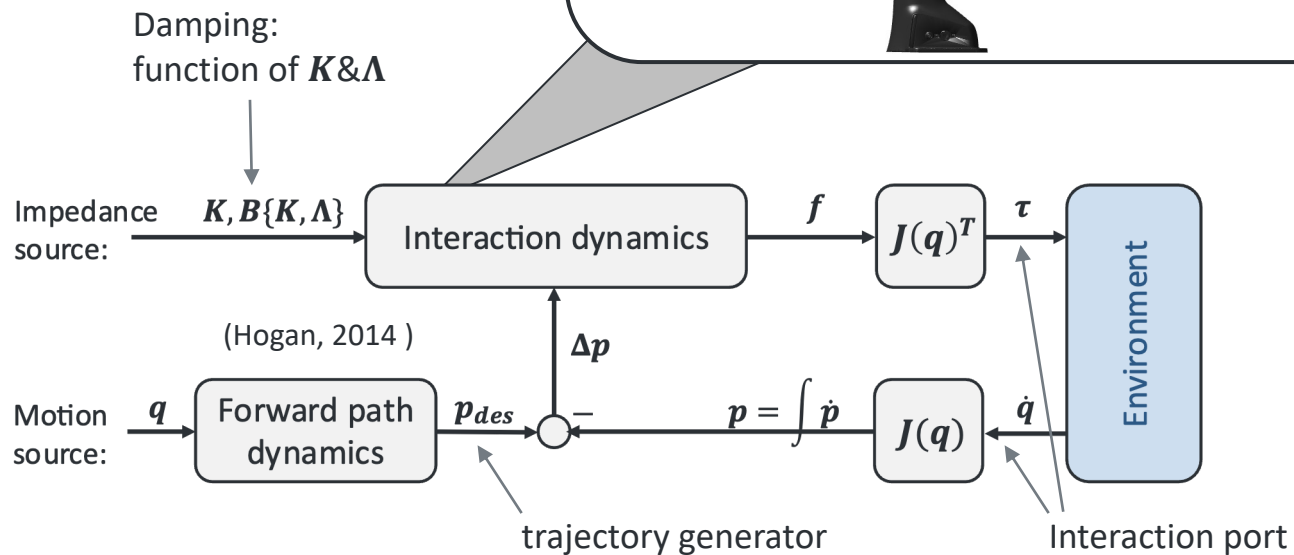
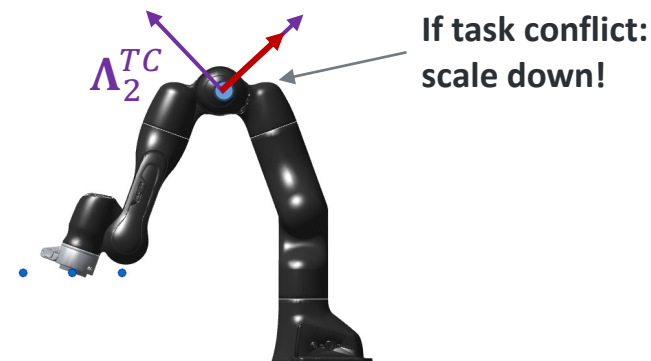
- Equivalent network structure of impedance control



Finding: Impedance shaping for multi-task control

- Equivalent network structure of impedance control

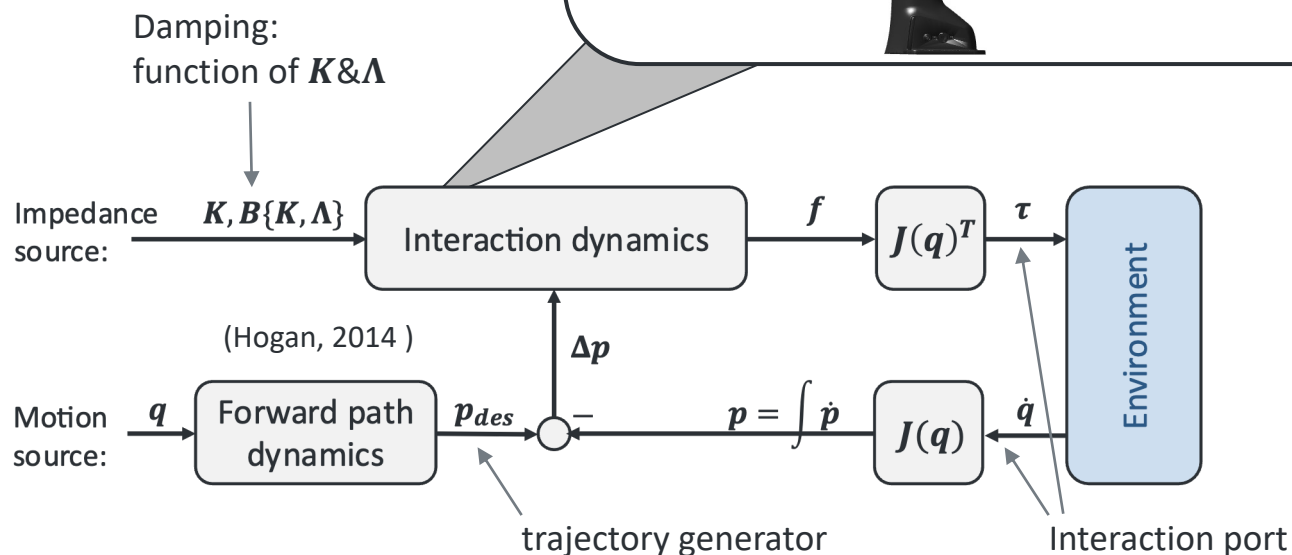
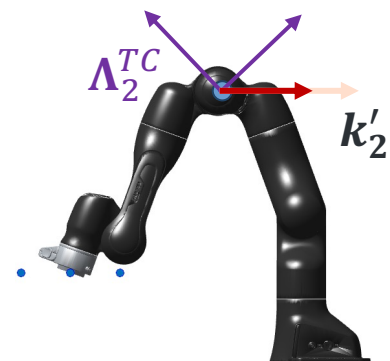
Shaping of subordinate task stiffness (Lachner et al., 2022):



Finding: Impedance shaping for multi-task control

- Equivalent network structure of impedance control

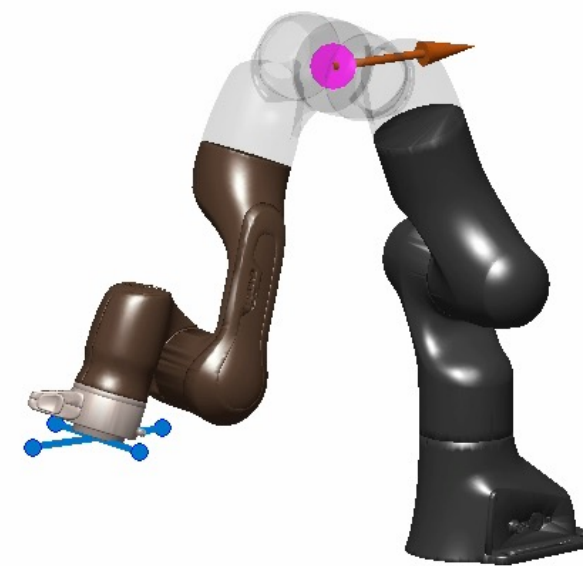
Shaping of subordinate task stiffness (Lachner et al., 2022):



Additional contributions:

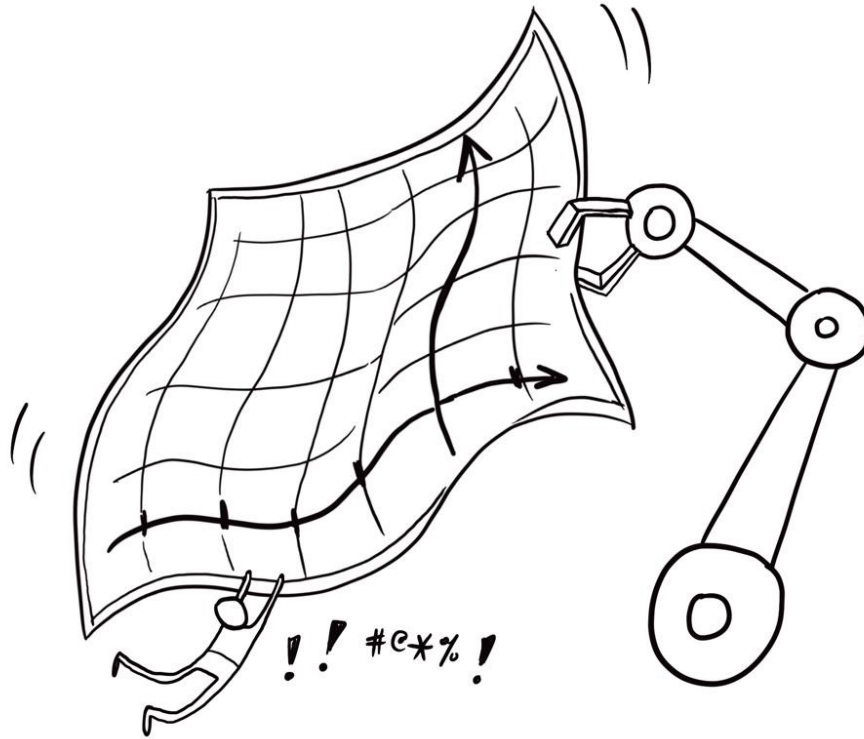
- Extension for rotational tasks
- Extension to multiple tasks
- Passivity layer
- Experiments on a real robot

$$k'_2 = 350 \text{ (kg/s}^2\text{)}$$



Impedance Shaping: solid
Impedance Superposition: transparent

IV. Safe physical Human-Robot Interaction



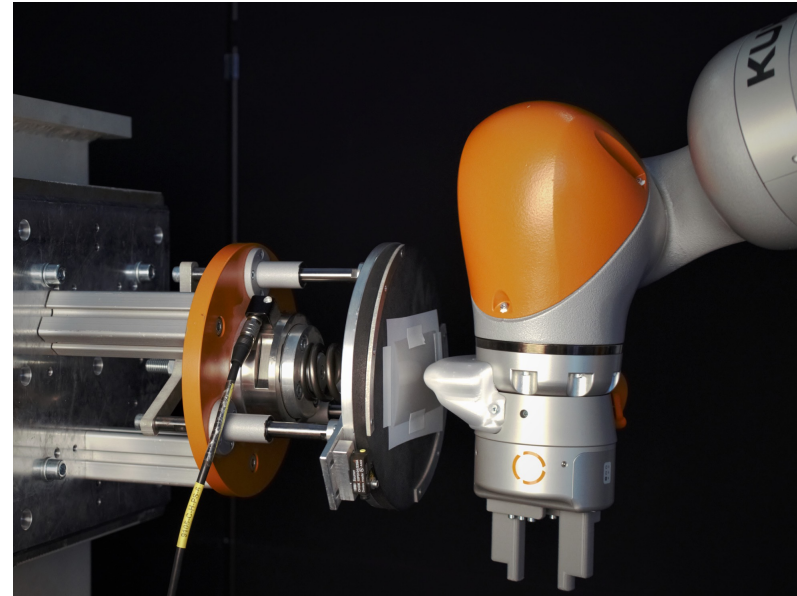
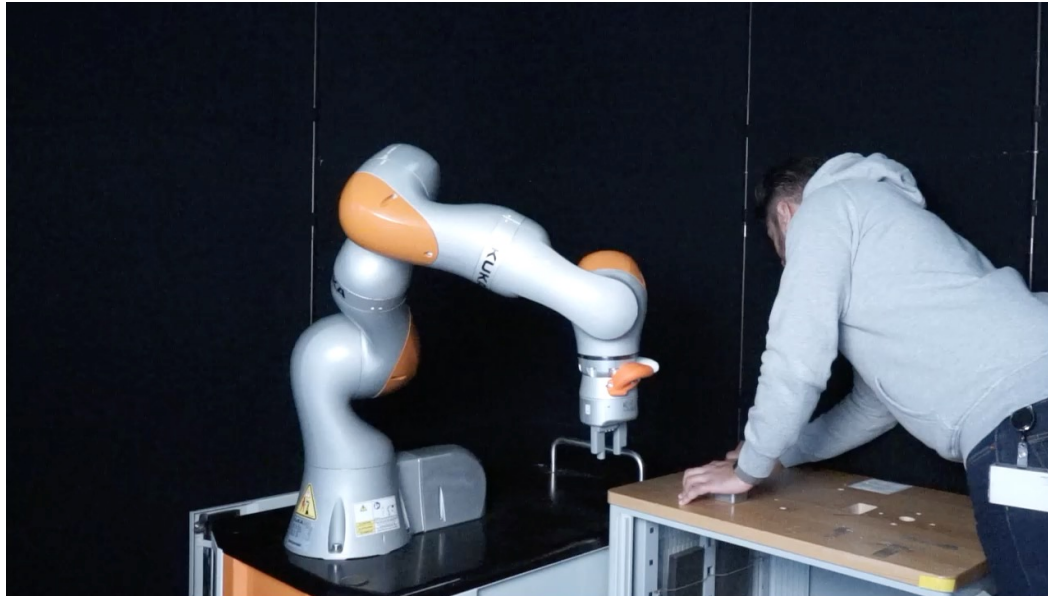
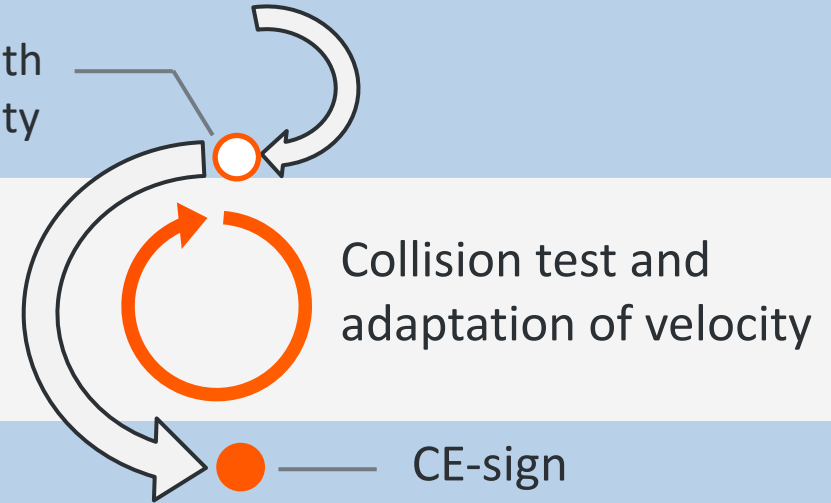
Problem statement: Coordinate dependency in industrial safety certification

Programming

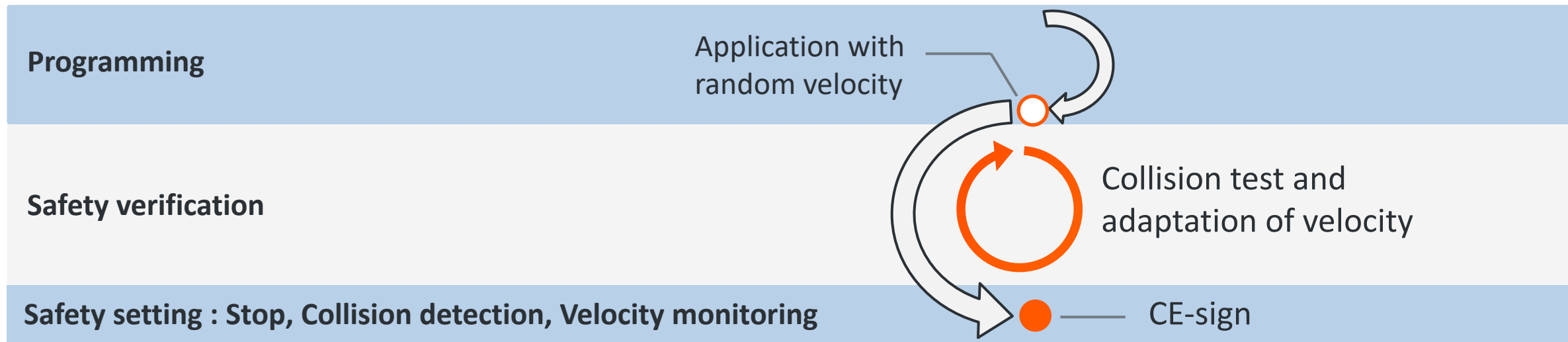
Application with
random velocity

Safety verification

Safety setting : Stop, Collision detection, Velocity monitoring

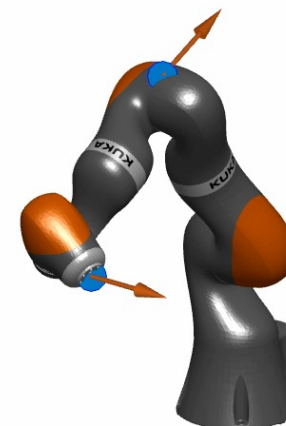
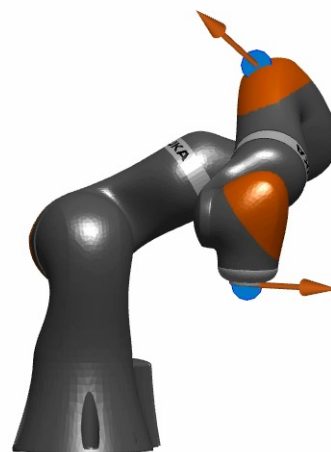
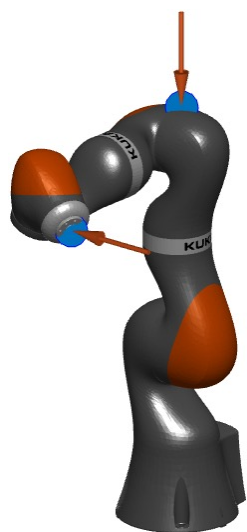


Problem statement: Coordinate dependency in industrial safety certification



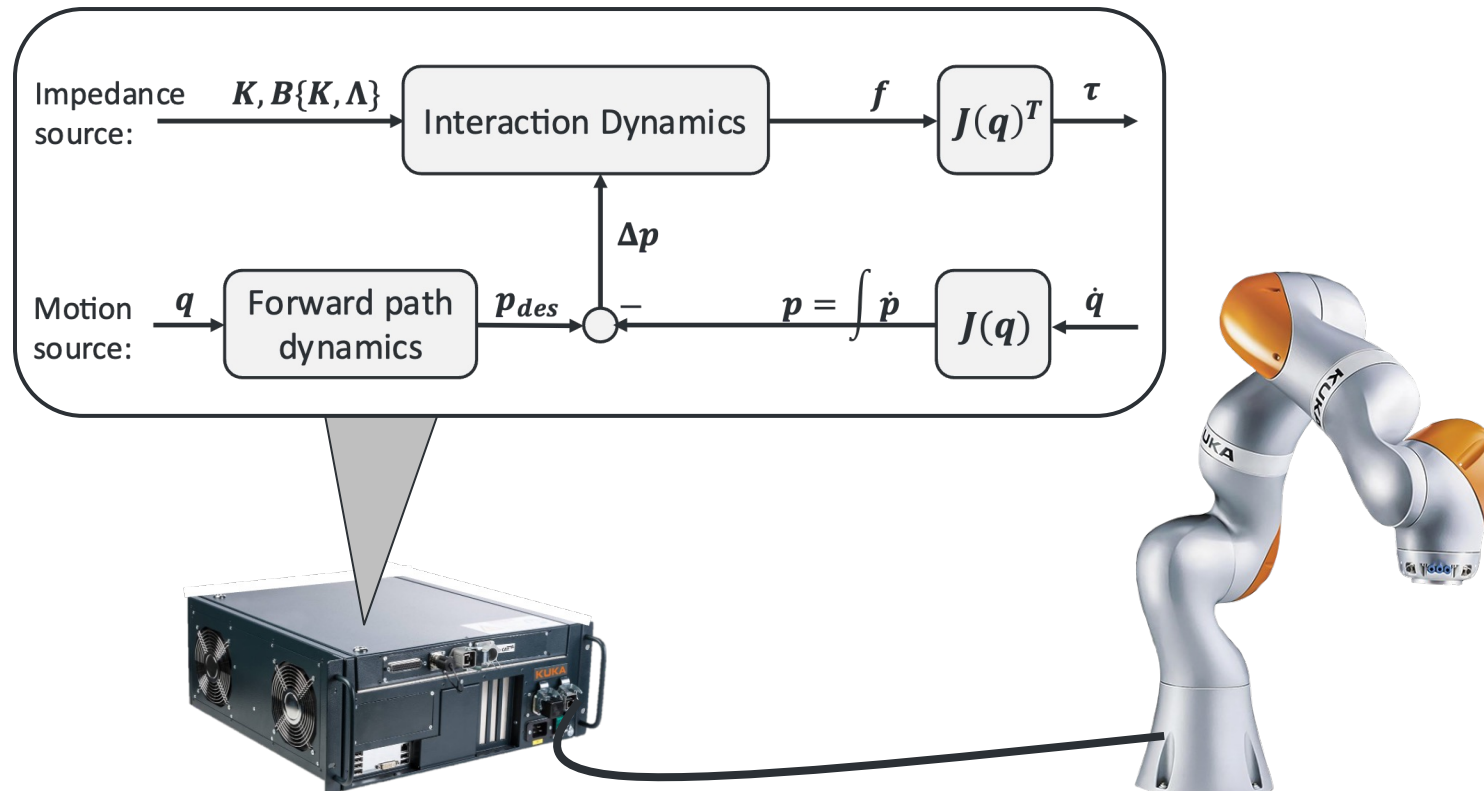
Max. velocity: $v_{ee} = 0$ (m/s) (End-Effector)

Elbow: $m_{refl} = 10.4187$ (kg)



Finding: Coordinate invariant robot control for safe physical interaction

- Controlled robotic system: Controller, Robot, Environment
- An Impedance Controller shapes the energy flow at the interaction port

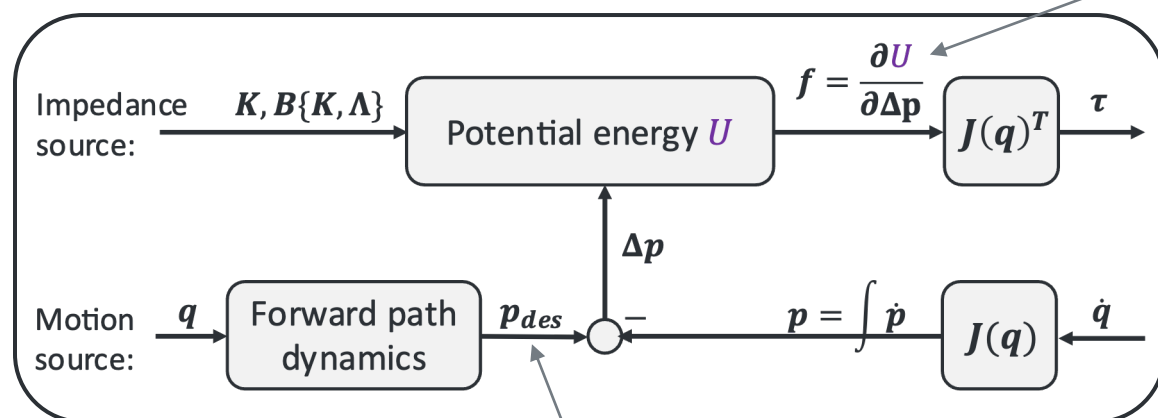


Finding: Coordinate invariant robot control for safe physical interaction

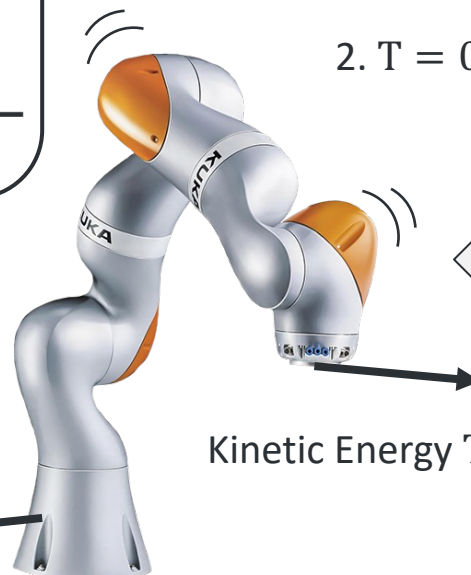
- Controlled robotic system: Controller, Robot, Environment
- An Impedance Controller shapes the energy flow at the interaction port
- Causality of energy flow:

We set an energy budget for $L = U + T$ (Lachner et al., 2021)
(defined by standards and regulations)

If violated, scale down U !



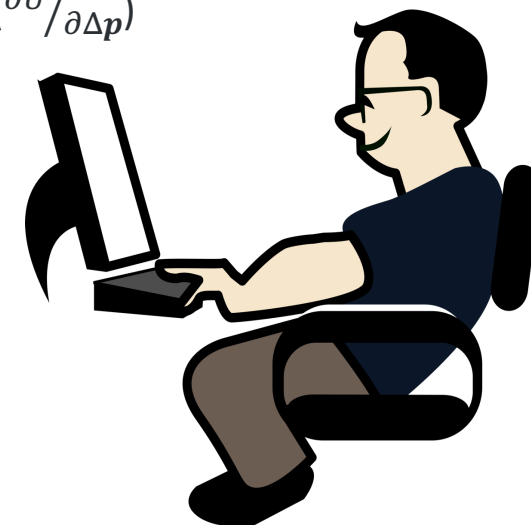
Pause trajectory
generator: $p_{des} = p$



Kinetic Energy T

1. $T \rightarrow$ Collision force

2. $T = 0 \rightarrow$ Clamping ($\frac{\partial U}{\partial \Delta p}$)

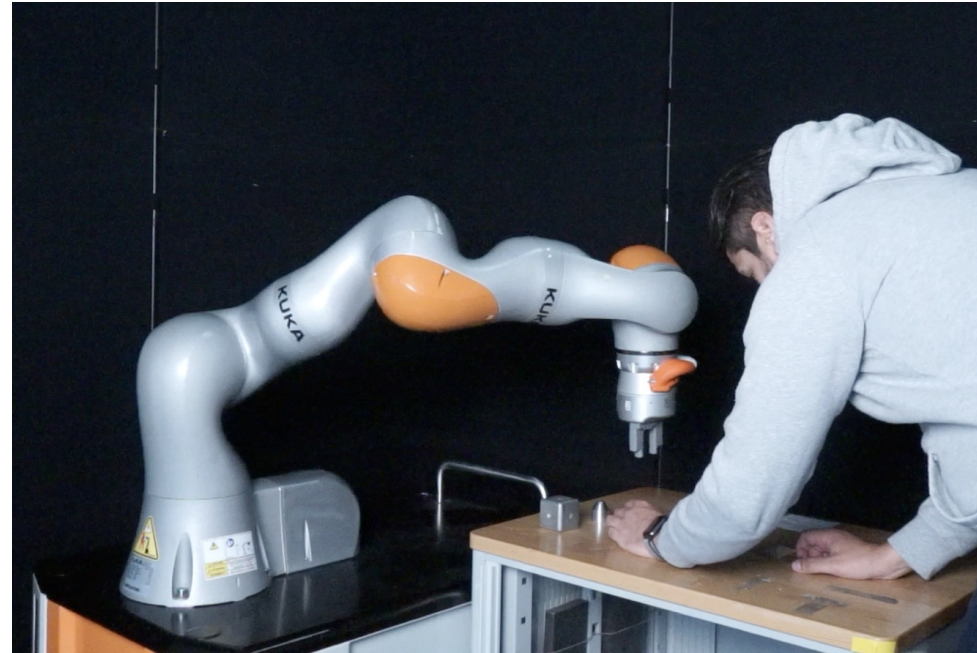


Finding: Coordinate invariant robot control for safe physical interaction

Interactive robot behavior



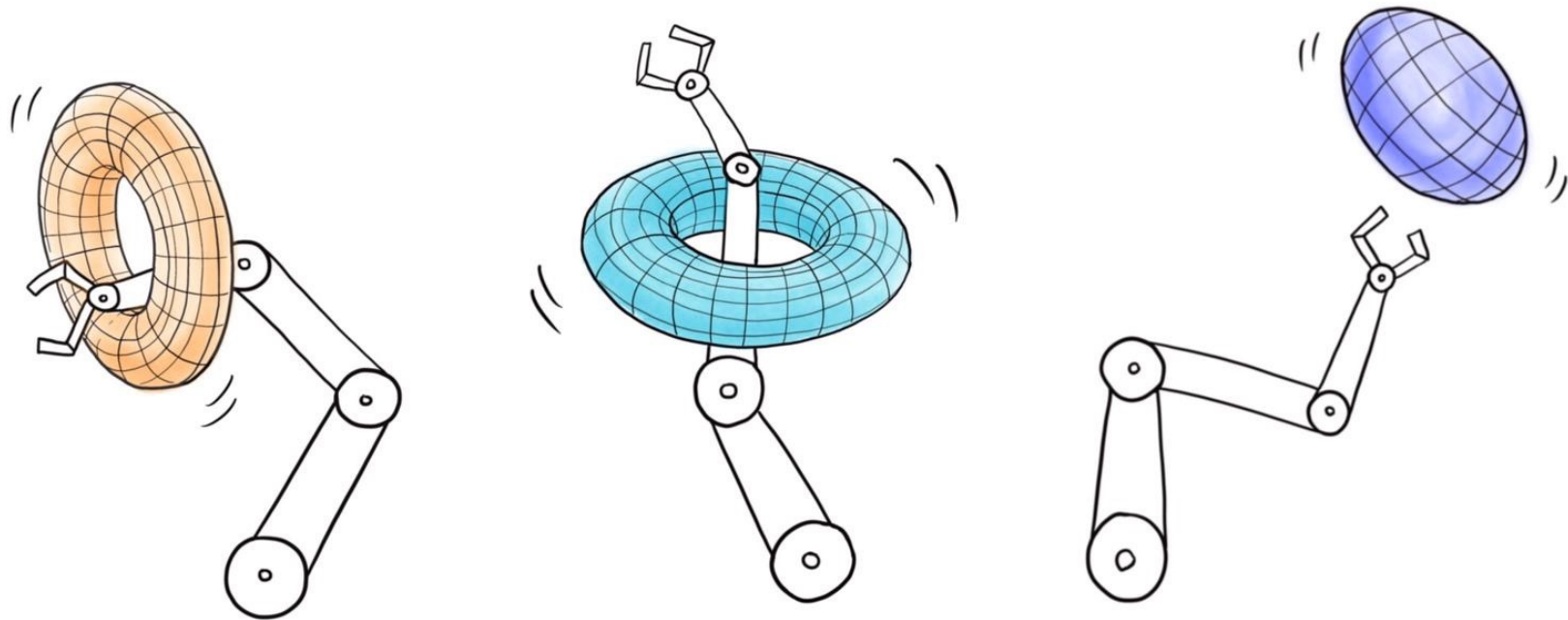
Resolving clamping dangers



Additional contributions:

- Safety verification with certified equipment
- Comparison with state-of-the-art methods

V. Summary of contributions



Contributions of the thesis

- Journal papers: Mechanism and Machine Theory, IEEE Transactions on Robotics (2x), International Journal of Robotics Research
- Conference papers: IEEE IROS (2x)
- Published patents (KUKA and UTwente)
 - <https://patents.google.com/patent/DE102019205651B3/>
 - <https://patents.google.com/patent/DE102020209866B3/>
 - <https://patents.google.com/patent/WO2017144682A1/>
- Transfer within KUKA
 - One algorithm part of an existing product
 - Used own algorithms to support two customer projects
 - Patented safety concept transferred to series development
- Software [EXP]licit[©]: Robot kinematics and dynamics based on Exponential Maps
 - Licensed and filed by MIT
 - The simulations (including code) of this presentation are available on GIT!
Link: <https://github.com/explicit-robotics/Explicit-MATLAB>

Thanks for your attention!

